

# ESTIMATION OF WARRANTY PERIOD FOR STRUCTURAL COMPONENTS OF AIRCRAFT

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**Abstract.** One of the most important problems in fatigue analysis and design of aircraft structures is the prediction of fatigue crack growth in service. Available in-service inspection data for various types of aircraft indicate that the fatigue crack damage accumulation in service involves considerable statistical variability. In this paper, we consider the problem of estimating the minimum time to crack initiation (or warranty period) for a number of aircraft structural components, before which no cracks (that may be detected) in materials occur, based on the results of previous warranty period tests on the structural components in question. This problem is a special case of a general class of problems concerned with the analysis of fatigue crack damage accumulation in aircraft service. The technique proposed here for solving this problem emphasizes pivotal quantities relevant for obtaining ancillary statistics. Attention is restricted to invariant families of distributions. Numerical examples are given.

**Keywords:** aircraft structures, fatigue cracks, warranty period, estimation.

## Introduction

Aircraft structures have many components. Maintaining high reliability for these structures generally requires that the individual structural components have

extremely high reliability, even after long periods of time. Prediction of fatigue crack growth in such components has not been an easy task. This is mainly because the manner in which the various parameters, such as loads, properties of materials and geometries of cracks, affect

the propagation of cracks is not clearly understood [2]. This, consequently, has led to a proliferation of hypotheses and laws for describing the propagation fatigue cracks [2, 9, 1]. Most of these models are based on concepts of the continuum theory with the assumption that cracks propagate in an ideal continuum media. Actual metallic materials, however, are composed of random microstructures described by various micro parameters, which can seriously affect the growth of a crack in these materials. As a result, the deterministic theories can only be accepted as an approximation of the actual random fatigue crack propagation process, which, broadly speaking, has five phases:

- 1) Dormant. There are no cracks in the materials.
- 2) Nucleation. The crack is initially formed.
- 3) Micro-crack growth. The crack grows rather haphazardly up to about 1 mm in length.
- 4) Macro-crack growth. The crack continues to propagate before its growth rate finally increases dramatically.
- 5) Failure. The component fails; this occurs very quickly relative to the other phases and can be ignored as a factor in determining reliability.

In the Fracture Mechanics approach to fatigue problems it is assumed that failure is caused by the unstable growth of a leading crack, which initiates, propagates, and reaches a critical size due to the fluctuations of the stress field around the crack tip. The transition from the initiation to the propagation stages corresponds to the distinction made between micro- and macro-cracks. Once a crack has attained a certain threshold size, failure occurs very rapidly. Thus, statistical fatigue life of structural components of aircraft may be divided, in general, into three stages, namely, crack nucleation, small crack growth, and large crack growth. Crack nucleation and small crack growth show a wide variation and hence a big spread on a cycles versus crack length graph. Relatively, large crack growth shows a lesser variation. Therefore, different models are fitted to the different stages of the fatigue evolution process, thus treating different stages as different phenomena. With these independent models, it is impossible to predict one phenomenon based on the information available about the other phenomenon. Experimentally, it is easier to carry out crack length measurements of large cracks compared to nucleating cracks and small cracks. Thus, it is easier to collect statistical data for large crack growth compared to the painstaking effort it would take to collect statistical data for crack nucleation and small crack growth.

We consider in this paper the problem of estimating the minimum time to crack initiation (warranty period or time to a first inspection) for a number of aircraft structural components, before which no cracks (that may be detected) in materials occur, based on the results of previous warranty period tests on the structural components in question. If in a fleet of  $k$  aircraft there are  $k_m$  of the same individual structural components, operating independently, the length of time until the first crack initially forms in any of these components is of basic interest and provides a measure of assurance

concerning the operation of the components in question. This leads to the consideration of the following problem. Suppose we have observations  $X_1, \dots, X_n$  as the result of tests conducted on the components; suppose also that there are  $k_m$  components of the same kind to be put into future use, with times to crack initiation  $Y_1, \dots, Y_{k_m}$ . Then we want to be able to estimate, on the basis of  $X_1, \dots, X_n$ , the shortest time to crack initiation  $Y_{(1,k_m)}$  among the times to crack initiation  $Y_1, \dots, Y_{k_m}$ . In other words, it is desirable to construct lower simultaneous prediction limit,  $L_\gamma$ , that is exceeded with probability  $\gamma$  by observations or functions of observations of all  $k$  future samples, each consisting of  $m$  units. In this paper, the problem of estimating  $Y_{(1,k_m)}$ , the smallest of all  $k$  future samples of  $m$  observations from the underlying distribution, based on an observed sample of  $n$  observations from the same distribution, is considered. A solution is proposed for constructing a lower simultaneous prediction limit,  $L_\gamma$ , for  $Y_{(1,k_m)}$ . Various properties of these solutions are derived, and illustrations are given for some important special cases.

The results have a direct application in reliability theory, where the time until the first failure in a group of  $m$  items in service provides a measure of assurance regarding the operation of the items.

In this paper, attention is restricted to invariant families of distributions. The technique used here emphasizes pivotal quantities relevant for obtaining ancillary statistics. It is a special case of the method of invariant embedding of sample statistics into a performance index applicable whenever the statistical problem is invariant under a group of transformations that acts transitively on the parameter space (i.e. in problems where there is a unique best invariant procedure) [4-7]. The analysis of the problem considered here is easily seen to be invariant under changes of location and scale.

## 1. Equation for constructing lower simultaneous one-sided prediction limits

An equation, which shows how to construct lower simultaneous one-sided prediction limits for the order statistics in all of future samples when a one-sided prediction limit for a single future sample is available, is given by the following theorem.

**Theorem 1.** Let  $(X_1, \dots, X_n)$  be a random sample from the cdf  $F(\cdot)$ , and let  $(Y_{1j}, \dots, Y_{m_jj})$  be the  $j$ th random sample of  $m_j$  "future" observations from the same cdf,  $j \in \{1, \dots, k\}$ . Assume that  $(k+1)$  samples are independent. Let  $H=H(X_1, \dots, X_n)$  be any statistic based on the preliminary sample and let  $Y_{(r_j, m_j)}$  denote the  $r_j$ th order statistic in the  $j$ th sample of size  $m_j$ . Then

$$\Pr\left(Y_{(i_1, m_1)} \geq H, \dots, Y_{(r_j, m_j)} \geq H, \dots, Y_{(i_k, m_k)} \geq H\right) = \sum_{i_1=0}^{n_1-1} \dots \sum_{i_j=0}^{r_j-1} \dots \sum_{i_k=0}^{n_k-1} \binom{m_1}{i_1} \dots \binom{m_j}{i_j}$$

$$\dots \binom{m_k}{i_k} \frac{\Pr(Y_{(i_\Sigma+1, m_\Sigma)} \geq H) - \Pr(Y_{(i_\Sigma, m_\Sigma)} \geq H)}{\binom{m_\Sigma}{i_\Sigma}}, \quad (1)$$

where

$$i_\Sigma = \sum_{j=1}^k i_j, \quad m_\Sigma = \sum_{j=1}^k m_j. \quad (2)$$

**Proof.**

$$\begin{aligned} & \Pr(Y_{(i_1, m_1)} \geq H, \dots, Y_{(i_j, m_j)} \geq H, \dots, Y_{(i_k, m_k)} \geq H) \\ &= \prod_{j=1}^k \Pr(Y_{(i_j, m_j)} \geq H) \\ &= E \left\{ \prod_{j=1}^k \sum_{i_j=0}^{m_j-1} \binom{m_j}{i_j} [F(H)]^{i_j} [1-F(H)]^{m_j-i_j} \right\} \\ &= \sum_{i_1=0}^{m_1-1} \dots \sum_{i_{j-1}=0}^{m_{j-1}-1} \dots \sum_{i_k=0}^{m_k-1} \binom{m_1}{i_1} \dots \binom{m_j}{i_j} \\ & \dots \binom{m_k}{i_k} E \left\{ [F(H)]^\Sigma [1-F(H)]^{m_\Sigma-i_\Sigma} \right\}. \end{aligned} \quad (3)$$

Since

$$\begin{aligned} & E \left\{ [F(H)]^\Sigma [1-F(H)]^{m_\Sigma-i_\Sigma} \right\} \\ &= \binom{m_\Sigma}{i_\Sigma}^{-1} E \left\{ \left[ \sum_{i=0}^{i_\Sigma} \binom{m_\Sigma}{i} [F(H)]^i [1-F(H)]^{m_\Sigma-i} \right] \right. \\ & \quad \left. - \sum_{i=0}^{i_\Sigma-1} \binom{m_\Sigma}{i} [F(H)]^i [1-F(H)]^{m_\Sigma-i} \right\} \\ &= \frac{\Pr(Y_{(i_\Sigma+1, m_\Sigma)} \geq H) - \Pr(Y_{(i_\Sigma, m_\Sigma)} \geq H)}{\binom{m_\Sigma}{i_\Sigma}}, \end{aligned} \quad (4)$$

The joint probability can be written as

$$\begin{aligned} & \Pr(Y_{(i_1, m_1)} \geq H, \dots, Y_{(i_j, m_j)} \geq H, \dots, Y_{(i_k, m_k)} \geq H) \\ &= \sum_{i_1=0}^{m_1-1} \dots \sum_{i_{j-1}=0}^{m_{j-1}-1} \dots \sum_{i_k=0}^{m_k-1} \binom{m_1}{i_1} \dots \binom{m_j}{i_j} \\ & \dots \binom{m_k}{i_k} \frac{\Pr(Y_{(i_\Sigma+1, m_\Sigma)} \geq H) - \Pr(Y_{(i_\Sigma, m_\Sigma)} \geq H)}{\binom{m_\Sigma}{i_\Sigma}}. \end{aligned} \quad (5)$$

This ends the proof.  $\square$

**Corollary 1.** If  $r_j = 1, \forall j=1(1)k$ , then

$$\begin{aligned} & \Pr(Y_{(1, m_1)} \geq H, \dots, Y_{(1, m_j)} \geq H, \dots, Y_{(1, m_k)} \geq H) \\ &= \Pr(Y_{(1, m_\Sigma)} \geq H). \end{aligned} \quad (6)$$

## 2. Invariant embedding technique for obtaining prediction limits

This paper is concerned with the implications of group theoretic structure for invariant performance indexes. We present an invariant embedding technique based on the constructive use of the invariance principle of mathematical statistics. This technique allows one to solve many problems of the theory of statistical inferences in a simple way. The aim of the present paper is to show how the invariance principle may be employed in the particular case of finding prediction limits. The technique used here is a special case of more general considerations applicable whenever the statistical problem is invariant under a group of transformations, which acts transitively on the parameter space.

### 2.1. Preliminaries

Our underlying structure consists of a class of probability models  $(\mathcal{X}, \mathcal{A}, \mathcal{P})$ , a one-one mapping  $\psi$  taking  $\mathcal{P}$  onto an index set  $\Theta$ , a measurable space of actions  $(\mathcal{U}, \mathcal{B})$ , and a real-valued function  $r$  defined on  $\Theta \times \mathcal{U}$ . We assume that a group  $G$  of one-one  $\mathcal{A}$ -measurable transformations acts on  $\mathcal{X}$  and that it leaves the class of models  $(\mathcal{X}, \mathcal{A}, \mathcal{P})$  invariant. We further assume that homomorphic images  $\bar{G}$  and  $\tilde{G}$  of  $G$  act on  $\Theta$  and  $\mathcal{U}$  respectively. ( $\bar{G}$  may be induced on  $\Theta$  through  $\psi$ ;  $\tilde{G}$  may be induced on  $\mathcal{U}$  through  $r$ ). We shall say that  $r$  is invariant if for every  $(\theta, u) \in \Theta \times \mathcal{U}$

$$r(\bar{g}\theta, \tilde{g}u) = r(\theta, u), \quad g \in G. \quad (7)$$

Given the structure described above there are aesthetic and sometimes admissibility grounds for restricting attention to decision rules  $\varphi: \mathcal{X} \rightarrow \mathcal{U}$ , which are  $(G, \tilde{G})$  equivariant in the sense that

$$\varphi(gx) = \tilde{g}\varphi(x), \quad x \in \mathcal{X}, \quad g \in G. \quad (8)$$

If  $\bar{G}$  is trivial and (7), (8) hold, we say  $\varphi$  is  $G$ -invariant, or simply invariant [5].

### 2.2. Invariant Functions

We begin by noting that  $r$  is invariant in the sense of (9) if and only if  $r$  is a  $G^\bullet$ -invariant function, where  $G^\bullet$  is defined on  $\Theta \times \mathcal{U}$  as follows: to each  $g \in G$ , with homomorphic images  $\bar{g}, \tilde{g}$  in  $\bar{G}, \tilde{G}$  respectively, let  $g^\bullet(\theta, u) = (\bar{g}\theta, \tilde{g}u)$ ,  $(\theta, u) \in (\Theta \times \mathcal{U})$ . It is assumed that  $\tilde{G}$  is a homomorphic image of  $\bar{G}$ .

**Definition 1 (Transitivity).** A transformation group  $\bar{G}$  acting on a set  $\Theta$  is called (uniquely) transitive if for every  $\theta, \vartheta \in \Theta$  there exists (unique)  $\bar{g} \in \bar{G}$  such that  $\bar{g}\theta = \vartheta$ .

When  $\bar{G}$  is transitive on  $\Theta$  we may index  $\bar{G}$  by  $\Theta$ : fix an arbitrary point  $\theta \in \Theta$  and define  $\bar{g}_{\theta_1}$  to be the unique  $\bar{g} \in \bar{G}$  satisfying  $\bar{g}\theta = \theta_1$ . The identity of  $\bar{G}$  clearly corresponds to  $\theta$ . An immediate consequence is Lemma 1.

**Lemma 1 (Transformation).** Let  $\bar{G}$  be transitive on  $\Theta$ . Fix  $\theta \in \Theta$  and define  $\bar{g}_{\theta_1}$  as above. Then  $\bar{g}_{\bar{q}\theta_1} = \bar{q}\bar{g}_{\theta_1}$  for  $\theta \in \Theta, \bar{q} \in \bar{G}$ .

**Proof.** The identity  $\bar{g}_{\bar{q}\theta_1}\theta = \bar{q}\theta_1 = \bar{q}\bar{g}_{\theta_1}\theta$  shows that  $\bar{g}_{\bar{q}\theta_1}$  and  $\bar{q}\bar{g}_{\theta_1}$  both take  $\theta$  into  $\bar{q}\theta_1$ , and the lemma follows by unique transitivity.

**Theorem 2 (Maximal Invariant).** Let  $\bar{G}$  be transitive on  $\Theta$ . Fix a reference point  $\theta_0 \in \Theta$  and index  $\bar{G}$  by  $\Theta$ . A maximal invariant  $M$  with respect to  $G^*$  acting on  $\Theta \times \mathcal{U}$  is defined by

$$M(\theta, u) = \bar{g}_{\theta_0}^{-1}u, \quad (\theta, u) \in \Theta \times \mathcal{U}. \quad (9)$$

**Proof.** For each  $(\theta, u) \in (\Theta \times \mathcal{U})$  and  $\bar{g} \in \bar{G}$

$$\begin{aligned} M(\bar{g}\theta, \bar{g}u) &= (\bar{g}_{\theta_0}^{-1}\bar{g}u) = (\bar{g}\bar{g}_{\theta_0}^{-1})^{-1}\bar{g}u \\ &= \bar{g}_{\theta_0}^{-1}\bar{g}^{-1}\bar{g}u = \bar{g}_{\theta_0}^{-1}u = M(\theta, u) \end{aligned} \quad (10)$$

by Lemma 1 and the structure preserving properties of homomorphisms. Thus  $M$  is  $G^*$ -invariant. To see that  $M$  is maximal, let  $M(\theta_1, u_1) = M(\theta_2, u_2)$ . Then  $\bar{g}_{\theta_1}^{-1}u_1 = \bar{g}_{\theta_2}^{-1}u_2$  or  $u_1 = \bar{g}u_2$ , where  $\bar{g} = \bar{g}_{\theta_1}\bar{g}_{\theta_2}^{-1}$ . Since  $\theta_1 = \bar{g}_{\theta_1}\theta_0 = \bar{g}_{\theta_1}\bar{g}_{\theta_2}^{-1}\theta_2 = \bar{g}\theta_2$ ,  $(\theta_1, u_1) = g^*(\theta_2, u_2)$  for some  $g^* \in G^*$ , and the proof is complete.

**Corollary 2.1 (Invariant Embedding).** An invariant function,  $r(\theta, u)$ , can be transformed as follows:

$$r(\theta, u) = r(\bar{g}_{\theta_0}^{-1}\theta, \bar{g}_{\theta_0}^{-1}u) = \check{r}(v, \eta), \quad (11)$$

where  $v = v(\theta, \hat{\theta})$  is a function (a pivotal quantity) such that the distribution of  $v$  does not depend on  $\theta$ ;  $\eta = \eta(u, \hat{\theta})$  is an ancillary factor;  $\hat{\theta}$  is the maximum likelihood estimator of  $\theta$  (or the sufficient statistic for  $\theta$ ).

**Corollary 2.2 (Best Invariant Decision Rule).** If  $r(\theta, u)$  is an invariant loss function, the best invariant decision rule is given by

$$\varphi^*(x) = u^* = \eta^{-1}(\eta^*, \hat{\theta}), \quad (12)$$

where

$$\eta^* = \arg \inf_{\eta} E_{\nu} \{ \check{r}(v, \eta) \}. \quad (13)$$

**Corollary 2.3 (Risk).** A risk function (performance index)

$$R(\theta, \varphi(x)) = E_x \{ r(\theta, \varphi(x)) \} = E_{\nu_0} \{ \check{r}(v_0, \eta_0) \} \quad (14)$$

is constant on orbits when an invariant decision rule  $\varphi(x)$  is used, where  $\nu_0 = \nu_0(\theta, x)$  is a function whose

distribution does not depend on  $\theta$ ;  $\eta_0 = \eta_0(u, x)$  is an ancillary factor.

For instance, consider the problem of estimating the location-scale parameter of a distribution belonging to a family generated by a continuous cdf  $F: \mathcal{P} = \{P_{\theta}: F((x-\mu)/\sigma), x \in \mathbb{R}, \theta \in \Theta\}$ ,  $\Theta = \{(\mu, \sigma): \mu, \sigma \in \mathbb{R}, \sigma > 0\} = \mathcal{U}$ . The group  $G$  of location and scale changes leaves the class of models invariant. Since  $\bar{G}$  induced on  $\Theta$  by  $P_{\theta} \rightarrow \theta$  is uniquely transitive, we may apply Theorem 2 and obtain invariant loss functions of the form

$$r(\theta, \varphi(x)) = r[(\varphi_1(x) - \mu)/\sigma, \varphi_2(x)/\sigma], \quad (15)$$

if  $\theta = (\mu, \sigma)$  and  $\varphi(x) = (\varphi_1(x), \varphi_2(x))$ . Let  $\hat{\theta} = (\hat{\theta}_1, \hat{\theta}_2)$ ,  $u = (u_1, u_2)$ , then

$$r(\theta, u) = \check{r}(v, \eta) = \check{r}(v_1 + \eta_1 v_2, \eta_2 v_2), \quad (16)$$

where  $v = (v_1, v_2)$ ,  $v_1 = (\hat{\theta}_1 - \mu)/\sigma$ ,  $v_2 = \hat{\theta}_2/\sigma$ ;  $\eta = (\eta_1, \eta_2)$ ,  $\eta_1 = (u_1 - \hat{\theta}_1)/\hat{\theta}_2$ ,  $\eta_2 = u_2/\hat{\theta}_2$ .

The invariant embedding technique, which is used for constructing lower simultaneous tolerance limits, is based on the result of Corollary 2.1.

### 3. Examples

**Example 1.** For instance, suppose that  $X_1, \dots, X_n$  and  $Y_{1j}, \dots, Y_{mj}$  ( $j=1, \dots, k$ ) denote  $n+km$  independent and identically distributed random variables from a left-truncated Weibull distribution with pdf

$$f(x; a, b, \delta) = \frac{\delta}{\sigma} x^{\delta-1} \exp\left[-(x^{\delta} - \mu^{\delta})/\sigma\right], \quad x \geq \mu, \sigma, \delta > 0, \quad (17)$$

which is characterized by being three-parameter  $(\mu, \sigma, \delta)$  where  $\delta$  is termed the shape parameter,  $\sigma$  is the scale parameter, and  $\mu$  is the truncation parameter interpreted as the minimum time to crack initiation (warranty period). It is assumed that the parameter  $\delta$  is known. Let  $X_{(1)}$  be the smallest observation in the initial sample of size  $n$  and

$$T_n = \sum_{i=1}^n (X_i^{\delta} - X_{(1)}^{\delta}). \quad (18)$$

It can be justified by using the factorization theorem that  $(X_{(1)}, T_n)$  is a sufficient statistic for  $(\mu, \sigma)$ . Let  $Y_{(1, m_j)}$  be the smallest observation in the  $j$ th future sample of size  $m_j = m, \forall j=1(1)k$ . We wish, on the basis of a sufficient statistic  $(X_{(1)}, T_n)$  for  $(\mu, \sigma)$ , to construct simultaneous one-sided lower  $100\gamma\%$  prediction limits for  $Y_{(1, m_j)}, j=1, \dots, k$ . It follows from Corollary 1 that this problem reduces to the problem of constructing a lower  $100\gamma\%$  prediction limit,  $L_{\gamma}$ , for

$$Y_{(1, km)} = \min_{1 \leq j \leq k} Y_{(1, m_j)}. \quad (19)$$

By using the above technique of invariant embedding of  $(X_{(1)}, T_n)$ , if  $X_{(1)} < Y_{(1, km)}$ , or  $(Y_{(1, km)}, T_n)$ , if

$X_{(1)} \geq Y_{(1,km)}$ , into a pivotal quantity  $(Y_{(1,km)}^\delta - \mu^\delta) / \sigma$  or  $(X_{(1)}^\delta - \mu^\delta) / \sigma$ , respectively, we obtain an ancillary statistic

$$W = (Y_{(1,km)}^\delta - X_{(1)}^\delta) / T_n \quad (20)$$

whose distribution does not depend on any unknown parameter. The pdf of  $W$  is given by

$$g(w) = \begin{cases} \frac{n(n-1)km}{n+km} \left(\frac{1}{1+kmw}\right)^n, & \text{if } w > 0, \\ \frac{n(n-1)km}{n+km} \left(\frac{1}{1-nw}\right)^n, & \text{if } w \leq 0. \end{cases} \quad (21)$$

Therefore, in this case  $L_\gamma$  can be found explicitly as

$$L_\gamma = \begin{cases} \left( X_{(1)}^\delta + \frac{T_n}{km} \left[ \left( \frac{n}{\gamma(n+km)} \right)^{\frac{1}{n-1}} - 1 \right] \right)^{1/\delta}, & \text{if } \frac{n}{n+km} > \gamma, \\ \left( X_{(1)}^\delta + \frac{T_n}{n} \left[ 1 - \left( \frac{km}{(1-\gamma)(n+km)} \right)^{\frac{1}{n-1}} \right] \right)^{1/\delta}, & \text{if } \frac{n}{n+km} \leq \gamma. \end{cases} \quad (22)$$

If, for instance,  $n=10$ ,  $\delta=8$ ,  $k=3$ ,  $m=5$ ,  $\gamma=0.95$ ,  $X_{(1)}=5$  (in number of  $10^4$  flight-hours), and  $T_n=10917240$ . Then we find from (22) that, with  $n/(n+km) = 10/(10+15) < \gamma$ ,

$$L_\gamma = \left( X_{(1)}^\delta + \frac{T_n}{n} \left[ 1 - \left( \frac{km}{(1-\gamma)(n+km)} \right)^{\frac{1}{n-1}} \right] \right)^{1/\delta} = \left( 5^8 + \frac{10917240}{10} \left[ 1 - \left( \frac{15}{(0.05)(10+15)} \right)^{\frac{1}{9}} \right] \right)^{1/8} = 3.8 \quad (23)$$

and we have 95% assurance that no cracks will occur in aircraft structural components before  $L_\gamma=3.8$  ( $\times 10^4$ ) flight-hours.

**Example 2.** Let  $X_{(1)} < X_{(2)} < \dots < X_{(r)}$  be the first  $r$  ordered observations of time to crack initiation for identical structural components of aircraft from a sample of size  $n$  from a two-parameter Weibull distribution with probability density function

$$f(x; \sigma, \delta) = \begin{cases} \frac{\delta}{\sigma} \left(\frac{x}{\sigma}\right)^{\delta-1} \exp[-(x/\sigma)^\delta], & x \geq 0, \\ 0, & \text{otherwise,} \end{cases} \quad (24)$$

where the parameters  $\sigma$  and  $\delta$  ( $\sigma > 0$ ,  $\delta > 0$ ) are unknown. Two types of censoring are generally recognized. In Type I censoring, the time, when censoring occurs, is fixed, and the number of survivors at this time are random variables. In Type II censoring, which is of primary interest here, the number of survivors is fixed and  $X_{(r)}$  is a random variable. In Type II censoring, the likelihood may be written as follows:

$$L \propto \left(\frac{\delta}{\sigma}\right)^r \left( \prod_{i=1}^r \left(\frac{x_{(i)}}{\sigma}\right)^{\delta-1} \right) \exp\left[-\sum_{i=1}^r \left(\frac{x_{(i)}}{\sigma}\right)^\delta\right] \times \left[ \int_{x_{(r)}}^{\infty} \frac{\delta}{\sigma} \left(\frac{x}{\sigma}\right)^{\delta-1} \exp[-(x/\sigma)^\delta] dx \right]^{n-r} \propto \left(\frac{\delta}{\sigma^\delta}\right)^r \left( \prod_{i=1}^r x_{(i)}^{\delta-1} \right) \exp\left[-\frac{1}{\sigma^\delta} \left[ \sum_{i=1}^r x_{(i)}^\delta + (n-r)x_{(r)}^\delta \right]\right], \quad (25)$$

$$\ln L = \text{constant} + r(\ln \delta - \delta \ln \sigma) + (\delta-1) \sum_{i=1}^r \ln x_{(i)} - \frac{\sum_{i=1}^r x_{(i)}^\delta + (n-r)x_{(r)}^\delta}{\sigma^\delta}. \quad (26)$$

This leads to the likelihood equations

$$\frac{\partial \ln L}{\partial \sigma} = -\frac{r\delta}{\sigma} + \frac{\sum_{i=1}^r x_{(i)}^\delta + (n-r)x_{(r)}^\delta}{\sigma^{2\delta}} \delta \sigma^{-\delta-1} = 0, \quad (27)$$

$$\frac{\partial \ln L}{\partial \delta} = \frac{r}{\delta} - r \ln \sigma + \sum_{i=1}^r \ln x_{(i)} - \left( \sum_{i=1}^r x_{(i)}^\delta \ln x_{(i)} + (n-r)x_{(r)}^\delta \ln x_{(r)} \right) \sigma^{-\delta} + \left( \sum_{i=1}^r x_{(i)}^\delta + (n-r)x_{(r)}^\delta \right) \sigma^{-\delta} \ln \sigma = 0. \quad (28)$$

Then the MLE's  $\hat{\sigma}$  and  $\hat{\delta}$  are solutions of

$$\hat{\sigma} = \left( \frac{\sum_{i=1}^r x_{(i)}^{\hat{\delta}} + (n-r)x_{(r)}^{\hat{\delta}}}{r} \right)^{1/\hat{\delta}}, \quad (29)$$

$$\hat{\delta} = \left[ \frac{\left( \sum_{i=1}^r x_{(i)}^{\hat{\delta}} \ln x_{(i)} + (n-r)x_{(r)}^{\hat{\delta}} \ln x_{(r)} \right)}{\left( \sum_{i=1}^r x_{(i)}^{\hat{\delta}} + (n-r)x_{(r)}^{\hat{\delta}} \right) - \frac{1}{r} \sum_{i=1}^r \ln x_{(i)}} \right]^{-1}. \quad (30)$$

The results given here apply to the Weibull distribution in the form (24). The results are presented more naturally, however, if we consider the variable  $\ln X$ , which follows the extreme-value distribution,

$$f(\ln x; a, b) = \frac{1}{b} \exp\left(\frac{\ln x - a}{b}\right) \exp\left(-\exp\left(\frac{\ln x - a}{b}\right)\right), \quad (31)$$

$-\infty < \ln x < \infty$ ,

where  $a = \ln \sigma$  and  $b = \delta^{-1}$ . Now (31) is a distribution with location and scale parameters  $a$  and  $b$ , and it is well known that if  $\hat{a}, \hat{b}$  are maximum likelihood estimates for  $a, b$  from a complete sample of size  $n$ , then  $(\hat{a}-a)/b, (\hat{a}-a)/\hat{b}$  and  $\hat{b}/b$  are quantities whose distributions depend only on  $n$ .

We are interested in estimating  $Y_{(1,km)}$ , the smallest order statistic in all  $k$  future samples, each consisting of  $m$  units from the distribution (24). It is easily shown that

$$W = (\ln Y_{(1)} - \hat{a})/\hat{b} = \hat{\delta}(\ln Y_{(1)} - \ln \hat{\sigma}) = \hat{\delta} \ln \left( \frac{Y_{(1)}}{\hat{\sigma}} \right), \quad (32)$$

where  $Y_{(1)} \equiv Y_{(1,km)}$ , is parameter-free, with distribution depending only on  $n$  and  $km$ . Hence, probability statements for  $V$  lead to confidence interval statements for  $Y_{(1)}$ .

Let  $X_{(1)}, X_{(2)}, \dots, X_{(n)}$  and  $Y_{(1)}, Y_{(2)}, \dots, Y_{(km)}$  represent ordered observations. In particular, let  $X_{(1)} < X_{(2)} < \dots < X_{(r)}$  be the first  $r$  ordered observations from a sample of size  $n$  from the distribution (24), i.e. we deal with Type II censoring. The joint density of  $\ln X_{(1)} \dots \ln X_{(r)}$  is

$$\begin{aligned} & f(\ln x_{(1)}, \dots, \ln x_{(r)}; a, b) \\ &= \frac{n!}{(n-r)!} \prod_{i=1}^r b^{-1} \exp \left( \frac{\ln x_{(i)} - a}{b} - \exp \left( \frac{\ln x_{(i)} - a}{b} \right) \right) \\ & \times \exp \left( -(n-r) \exp \left( \frac{\ln x_{(r)} - a}{b} \right) \right). \end{aligned} \quad (33)$$

Let  $\hat{a}, \hat{b}$  be the maximum likelihood estimators of  $a, b$ , based on  $X_{(1)}, \dots, X_{(r)}$ , and let  $V_1 = (\hat{a} - a)/b, V_2 = \hat{b}/b$ , and  $\cdot W_i = (\ln X_{(i)} - \hat{a})/\hat{b} (i=1, \dots, r)$ . It is easily shown that the distributions of  $V_1, V_2$  are parameter-free, and that any  $r-2$  of the  $\cdot W_i$ 's, say  $\cdot W_1, \dots, \cdot W_{r-2}$ , form a set of  $r-2$  functionally independent ancillary statistics. We then find in a straightforward manner that the joint density of  $V_1, V_2$ , conditional on fixed  $\cdot W = (\cdot W_1, \dots, \cdot W_{r-2})$ , is

$$\begin{aligned} & f(v_1, v_2; \cdot w_1, \dots, \cdot w_{r-2}) \\ &= \mathcal{Q}(\cdot w) v_2^{r-2} \exp \left( r v_1 + v_2 \sum_{i=1}^r \cdot w_i - \sum_{i=1}^r \exp(v_1 + \cdot w_i v_2) \right) \\ & \quad \left( -(n-r) \exp(v_1 + \cdot w_i v_2) \right) \end{aligned} \quad (34)$$

where  $\mathcal{Q}(\cdot w)$  is a normalizing constant. For notational convenience we include all of  $\cdot w_1, \dots, \cdot w_r$  in (34);  $\cdot w_{r-1}$  and  $\cdot w_r$  can be expressed as function of  $\cdot w_1, \dots, \cdot w_{r-2}$  only.

Let  $Y_{(1)}$  be the smallest observation from an independent second sample of  $km$  observations also from the distribution (24). Writing  $V = (\ln Y_{(1)} - a)/b$  and noting that  $\exp(V)$  is the smallest observation in a sample of size  $km$  from the standard exponential distribution, we have the density of  $V$  as

$$f(v) = km \exp(v) \exp(-km \exp(v)). \quad (35)$$

Since  $V$  is distributed independently of  $V_1, V_2$  we find the joint density of  $V, V_1, V_2$ , conditional on  $\cdot W = \cdot w$ , as the product of (34) and (35). Note that  $W = (\ln Y_{(1)} - \hat{a})/\hat{b} = (V - V_1)/V_2$ ; making the transformation  $W = (V - V_1)/V_2, V_1 = V_1, V_2 = V_2$ , we find the joint density of  $W, V_1, V_2$ , conditional on  $\cdot W = \cdot w$ , as

$$\begin{aligned} & f(w, v_1, v_2; \cdot w) \\ &= km \mathcal{Q}(\cdot w) \exp \left( (r+1)v_1 + \left( w + \sum_{i=1}^r \cdot w_i \right) v_2 \right) \\ & \times \exp[-km \exp(v_1 + wv_2)] \\ & \times \exp \left( -\exp(v_1) \left( \sum_{i=1}^r \exp(\cdot w_i v_2) + (n-r) \exp(\cdot w_i v_2) \right) \right). \end{aligned} \quad (36)$$

Now  $v_1$  can be integrated out of (36) in a straightforward way to give

$$\begin{aligned} & f(w, v_2; \cdot w) \\ &= \frac{km \mathcal{Q}(\cdot w) v_2^{r-1} \exp \left( \left( w + \sum_{i=1}^r \cdot w_i \right) v_2 \right)}{\left( km \exp(wv_2) + \sum_{i=1}^r \exp(\cdot w_i v_2) + (n-r) \exp(\cdot w_r v_2) \right)^{r+1}}. \end{aligned} \quad (37)$$

Consider, for fixed  $w (-\infty < w < \infty)$ ,

$$\Pr\{W > w; \cdot w\} = \int_0^\infty \int_w^\infty f(w, v_2; \cdot w) dw dv_2. \quad (38)$$

A straightforward integration then gives us

$$\begin{aligned} \Pr\{W > w; \cdot w\} &= \Pr \left\{ \hat{\delta} \ln \left( \frac{Y_{(1)}}{\hat{\sigma}} \right) > w; \cdot w \right\} \\ &= \left( \int_0^\infty s^{r-2} e^{-s \hat{\delta} \sum_{i=1}^r \ln(x_{(i)}/\hat{\sigma})} \right. \\ & \quad \left. \times \left( km e^{sw} + \sum_{i=1}^r e^{-s \hat{\delta} \ln(x_{(i)}/\hat{\sigma})} + (n-r) e^{-s \hat{\delta} \ln(x_{(r)}/\hat{\sigma})} \right)^{-r} ds \right) \\ & \times \left( \int_0^\infty s^{r-2} e^{-s \hat{\delta} \sum_{i=1}^r \ln(x_{(i)}/\hat{\sigma})} \left( \sum_{i=1}^r e^{-s \hat{\delta} \ln(x_{(i)}/\hat{\sigma})} + (n-r) e^{-s \hat{\delta} \ln(x_{(r)}/\hat{\sigma})} \right)^{-r} ds \right)^{-1}. \end{aligned} \quad (39)$$

The above expression holds for  $3 \leq r \leq n$ , with  $r=n$  corresponding to complete (uncensored) sampling. In the case  $r=2$ ,  $\hat{a}, \hat{b}$  are jointly sufficient for  $a, b$ , so that it can be considered the unconditional probability  $\Pr(W > w)$ . It will be noted that in this case, the correct expression is also given by (39), with  $r=2$ . Now the probability statement

$$\Pr\left\{\widehat{\delta}\ln\left(\frac{Y_{(1)}}{\widehat{\sigma}}\right) > w; \bullet \mathbf{w}\right\} = \gamma \tag{40}$$

leads to the warranty period  $(0, \widehat{\sigma}\exp(w/\widehat{\delta}))$  with confidence level  $\gamma$ , i.e. a lower  $100\gamma\%$  prediction limit,  $L_\gamma$ , for  $Y_{(1)}$  is equal to  $\widehat{\sigma}\exp(w/\widehat{\delta})$ .

For instance, consider the data of fatigue tests on a particular type of structural component of the aircraft IL-86. The data are for a complete sample of size  $r = n = 5$ , with observations

**Table.** The Data of Fatigue Tests on a Particular Type of Structural Component of IL-861 Aircraft

Observations	Time to crack initiation (in number of $10^4$ flight-hours)
$x_{(1)}$	5
$x_{(2)}$	6.25
$x_{(3)}$	7.5
$x_{(4)}$	7.9
$x_{(5)}$	8.1

The results are being expressed here in number of  $10^4$  flight-hours. On the basis of these data, the wish is to estimate a lower 0.95 prediction limit on  $Y_{(1)}$  in a group of  $m = 5$  identical components (for a fleet of  $k=1$  IL-86 aircraft) that are to be put into service.

**Goodness-of-fit testing.** We assess the statistical significance of departures from the Weibull model by performing the empirical distribution function goodness-of-fit test. We use the S statistic [3]. For censoring (or complete) data sets, the S statistic is given by

$$S = \frac{\sum_{i=[r/2]+1}^{r-1} \left(\frac{\ln(x_{(i+1)}/x_{(i)})}{M_i}\right)}{\sum_{i=1}^{r-1} \left(\frac{\ln(x_{(i+1)}/x_{(i)})}{M_i}\right)} = \frac{\sum_{i=3}^4 \left(\frac{\ln(x_{(i+1)}/x_{(i)})}{M_i}\right)}{\sum_{i=1}^4 \left(\frac{\ln(x_{(i+1)}/x_{(i)})}{M_i}\right)} = 0.184, \tag{41}$$

where  $[r/2]$  is a largest integer  $\leq r/2$ , the values of  $M_i$  are given in Table 13 [3]. The reject region for the  $\alpha$  level of significance is  $\{S > S_{n,1-\alpha}\}$ . The percentage points for  $S_{n,1-\alpha}$  were given by Kapur and Lamberson [3]. For this example,

$$S=0.184 < S_{n=5, 1-\alpha=0.95}=0.86. \tag{42}$$

Thus, there is no evidence to rule out the Weibull model.

The maximum likelihood estimates are  $\widehat{\sigma} = 7.42603$  and  $\widehat{\delta} = 7.9081$ . It follows from (39) that

$$\Pr\left\{\widehat{\delta}\ln\left(\frac{Y_{(1)}}{\widehat{\sigma}}\right) > -4.55761\right\} = \frac{0.000016192}{0.0000170442} = 0.95 \tag{43}$$

and a lower 0.95 prediction limit for  $Y_{(1)}$  is 4.1730 ( $\times 10^4$ ) flight-hours, i.e. we have obtained the warranty period equal to 41730 flight-hours with confidence level  $\gamma=0.95$ .

## Conclusions

In this paper we consider the important situation in which it can be assumed that the structural components of the aircraft in question have the time to crack initiation following the Weibull distribution. It will be noted that the general problem considered here, that of predicting on the basis of an ordered sample the smallest observation  $Y_{(1,km)}$  from  $k$  future samples, each consisting of  $m$  units, has application in reliability theory other than described above. For example, if one has a series system consisting of  $m$  identical components, with lifetimes  $Y_1, \dots, Y_m$ , then  $Y_{(1)} \equiv Y_{(1,m)}$  represents the life of the system; it is often wished to estimate  $Y_{(1)}$  for a given system, on the basis of previous life test data on the components.

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## References

1. **Chand S., Garg S.B.L.** Propagation Under Constant Amplitude Loading // Engineering Fracture Mechanics. – 1985. – Vol. 21. – P. 1–30.
2. **Hoeppner D.W., Krupp W.E.** Prediction of Component Life by Application of Fatigue Crack Growth Knowledge // Engineering Fracture Mechanics. – 1974. – Vol. 6. – P. 47–70.
3. **Kapur K.C., Lamberson L.R.** Reliability in Engineering Design. – John Wiley & Sons, 1977.
4. **Nechval N.A.** Modern Statistical Methods of Operations Research. – Riga: RCAEI, 1982.
5. **Nechval N.A.** Theory and Methods of Adaptive Control of Stochastic Processes. – Riga: RCAEI, 1984.
6. **Nechval N.A., Nechval K.N.** State Estimation of Stochastic Systems via Invariant Embedding
7. Technique // Cybernetics and Systems'2000 / Edited by R. Trappl. – Vienna: Austrian Society for Cybernetic Studies, 2000. – Vol. 1. – P. 96–101.
8. **Nechval N.A., Nechval K.N., Vasermanis E.K.** Invariant Embedding Technique and its Applications to Statistical Decision-Making // Proceedings of the Second World Congress of Latvian Scientists. – Riga: LZP, 2001. – P. 578.
9. **Nechval N.A., Nechval K.N., Vasermanis E.K.** Optimization of Interval Estimators via Invariant Embedding Technique // IJCAS (International Journal of Computing Anticipatory Systems). – 2001. – Vol 9. – P. 241–255.
10. **Schwalbe K-H.** Comparison of Several Fatigue Crack Propagation Laws With Experimental Results // Engineering Fracture Mechanics. – 1974. – Vol 6. – P. 325–341.